### Using the PO3 Precession Model

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Systèmes de Référence Temps-Espace

## Improving the IAU 2000 precession

- The precession part of the IAU 2000A bias-precession-nutation model consists simply of rate adjustments to the former precession model, IAU 1976. This "IAU 2000 precession" fits the existing VLBI observations well, but is not consistent with dynamical theory beyond first order.
- To improve on IAU 2000, what was needed:
  - A new model for the precession of the ecliptic.
  - A model for the precession of the equator consistent with dynamical theories.
- The replacement precession model that has been chosen by the IAU WG Precession and the Ecliptic (James Hilton, chair) is the "PO3" solution of Capitaine et al. (2003).
- In addition to the new precession models for ecliptic and equator, PO3 includes:
  - Slight adjustments to the nutation model.
  - ullet A parameterized solution to prepare for future revisions of precession and  $J_2$  rates.
- Subject to IAU resolution, PO3-based precession-nutation procedures will be needed for the IERS Conventions (and the SOFA software).

### P03 precession

- The PO3 precession of the ecliptic is based on a fit to DE406 over a 2000-year interval, after removal of periodic terms using VSOP87.
- The PO3 precession of the equator is based on semi-analytical integration of the Earth's precession equations, and is consistent with non-rigid Earth models.
- PO3 has been verified by comparing with VLBI observations 1985-2005, with FCN taken into account.

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Capitaine N., Wallace P.T., Chapront J. (2003, A&A 412, 567-586)

"Expressions for IAU 2000 precession quantities"

the P03 solution for the precession of the ecliptic and the precession of the equator

Capitaine N., Wallace P.T., Chapront J. (2004, A&A 421, 365-379)

"Comparison between high precision precession models for the ecliptic and the equator"

comparison between the recent precession models P03/B03/F03/HF04/IAU 2000

Capitaine N., Wallace P.T., Chapront J. (2004, A&A 432, 355-367)

"Improvement of the IAU 2000 precession model"

fit to VLBI, P03 Tables and the parameterized "P04_par" precession solution

Capitaine N., Wallace P.T., (2006, A&A 450, 855-872)

"High precision methods for locating the celestial intermediate pole and origin"

comparison of the different ways of locating the (P03) CIP and CIO

Wallace P.T., Capitaine N., (2006, submitted to A&A)

"Precession-nutation procedures consistent with IAU 2006 resolutions"
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precession-nutation procedures suitable for (i) SOFA and (ii) IERS Conventions, and (iii) concise method

#### PO3 adjustments to IAU 2000A nutation

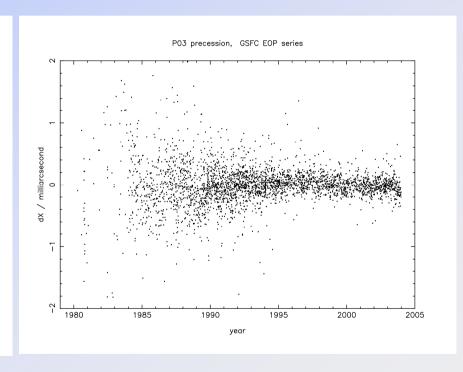
- For use with PO3 precession, slight adjustments to the IAU 2000A nutation are needed:
  - Change of nutation amplitudes (in longitude only) to take account of the revised obliquity: a geometrical effect.
  - Change of nutation amplitudes (in both longitude and obliquity) due to the secular variation of the Earth's dynamical flattening: not considered in IAU 2000A.
- The adjustments are (at present) small: a few microarcseconds.

#### Fits of IAU2000 and PO3 to VLBI: X

#### IAU 2000

# AU 2000 precession, GSFC EOP series RAU 2000 precession, GSFC EOP series 1980 1985 1990 1995 2000 2005

#### P03

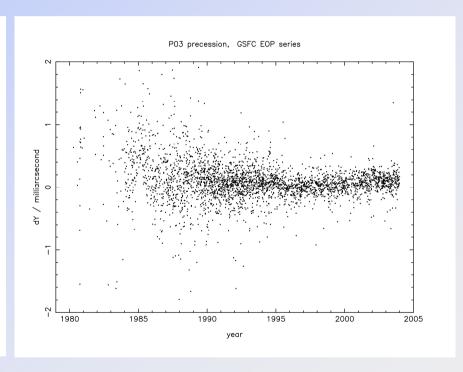


#### Fits of IAU2000 and PO3 to VLBI: Y

#### IAU 2000

# NAU 2000 precession, GSFC EOP series Representation of the property of the pr

#### P03



# Building-blocks

- The goal is to generate these matrices:
  - GCRS RCIRS (or GCRS Rtrue)
  - GCRS RTIRS
- This can be done if we know these vectors:
  - V<sub>CIP</sub>
  - v<sub>CIO</sub> (or v<sub>equinox</sub>)
- ...and this angle:
  - ERA (or GST)
- The equation of the origins links classical and new:
  - EO = ERA-GST = distance from CIO to equinox

## Forming the GCRS-to-TIRS matrix

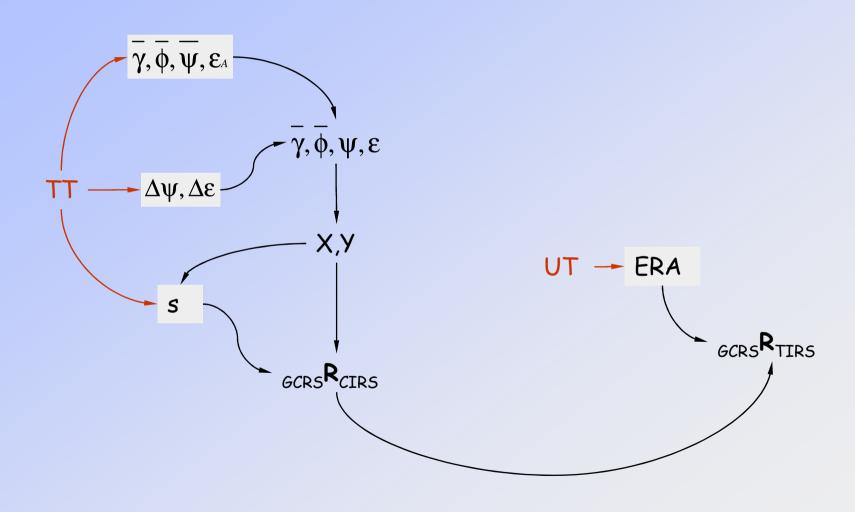
$$GCRSRTIRS = R_3(ERA) \times \begin{pmatrix} \mathbf{v}_{CIO} \\ \mathbf{v}_{CIP} \times \mathbf{v}_{CIO} \\ \mathbf{v}_{CIP} \end{pmatrix} = R_3(GST) \times \begin{pmatrix} \mathbf{v}_{equinox} \\ \mathbf{v}_{CIP} \times \mathbf{v}_{equinox} \\ \mathbf{v}_{CIP} \end{pmatrix}$$

$$= ERA - EO$$

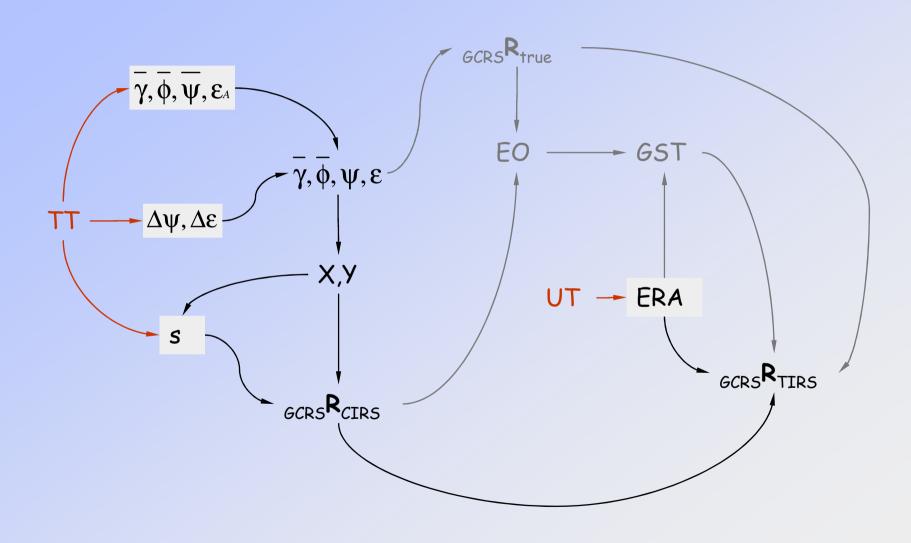
# Algorithm choices

- The *Precession and the Ecliptic WG* report leaves open the choice of parameterization.
- Capitaine and Wallace (2006) describes:
  - $\bullet$  6 ways of forming  $_{GCRS}R_{CIRS}$
  - lacksquare 3 ways of obtaining  $oldsymbol{v}_{CIP}$
  - 8 ways of obtaining  $\mathbf{v}_{CIO}$
- Different applications have different priorities. For example:
  - A general-purpose toolkit such as SOFA must
    - have a clear provenance
    - be versatile, concise and efficient
    - be highly self-consistent
  - IERS Conventions addresses a demanding but highly focused application:
    - it must be straightforward to use
    - it must perform efficiently and accurately
  - In many applications accuracy can be traded off against size and speed.
- Wallace and Capitaine (2006, submitted):
  - Concentrates on two specific choices.
  - Provides detailed numerical examples.

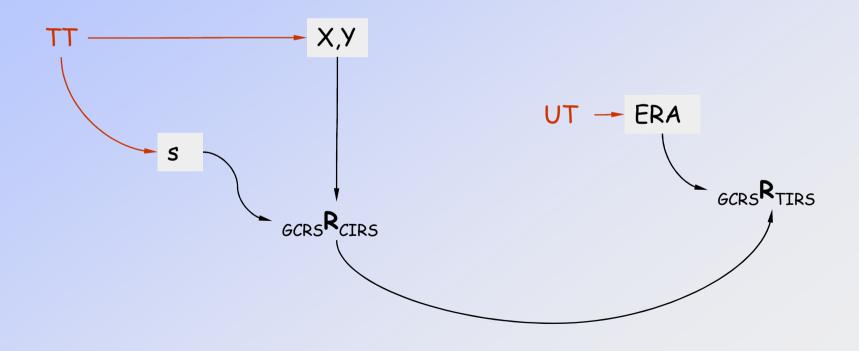
# "Angles" method



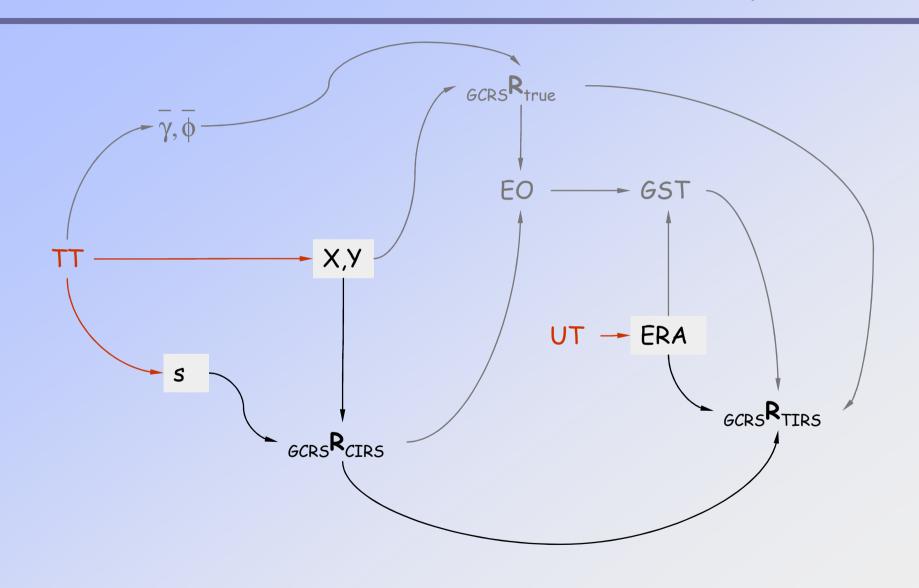
# "Angles" method - equinox option



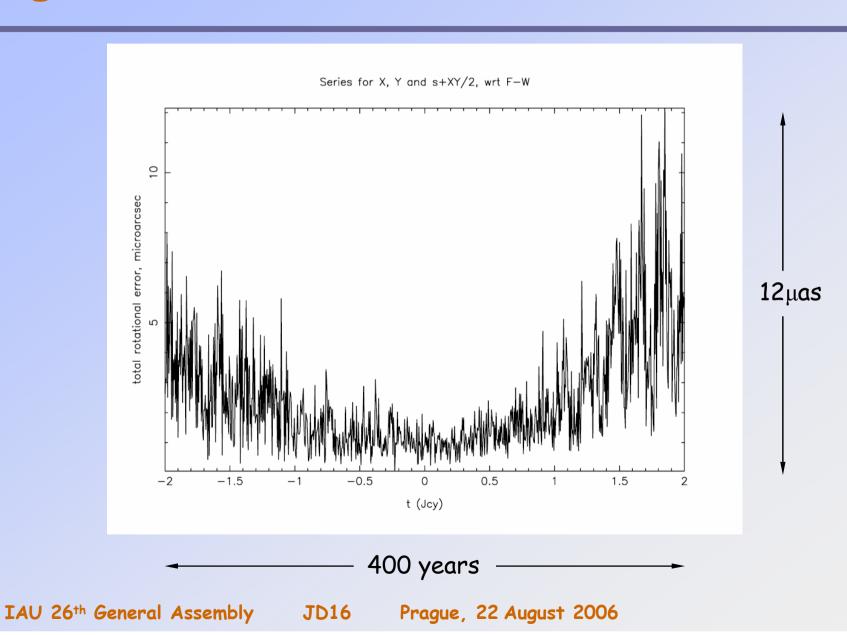
# "X,Y series" method



# "X,Y series" method - equinox option



#### Agreement between the two methods



# The series compared

		number of terms					
		1	†	<i>†</i> 2	<i>†</i> <sup>3</sup>	<i>†</i> <sup>4</sup>	<b>†</b> 5
angles / nethod	$-\frac{1}{\gamma}$	1	1	1	1	1	1
	$\overline{\phi}$	1	1	1	1	1	1
	Ψ	1321	38	1	1	1	1
	<b>E</b> A	1038	20	1	1	1	1
X,Y nethod	X	1307	254	37	5	2	1
	Y	963	278	31	6	2	1
both	s + XY/2	34	4	26	5	2	1

# Approximate GCSR RTIRS matrices

$$\begin{pmatrix} \cos s + X(Y\sin s - X\cos s)/(1+Z) & -\sin s + Y(Y\sin s - X\cos s)/(1+Z) & -(X\cos s - Y\sin s) \\ \sin s - X(Y\cos s + X\sin s)/(1+Z) & \cos s - Y(Y\cos s + X\sin s)/(1+Z) & -(Y\cos s + X\sin s) \\ X & Y & Z \end{pmatrix}$$
rigorous

$$\begin{pmatrix}
1 - \frac{X^2}{2} & -s - \frac{XY}{2} & -X \\
s - \frac{XY}{2} & 1 - \frac{Y^2}{2} & -Y - sX \\
X & Y & 1 - \frac{(X^2 + Y^2)}{2}
\end{pmatrix}$$

$$\begin{pmatrix} 1 - \frac{X^2}{2} & -s - \frac{XY}{2} & -X \\ s - \frac{XY}{2} & 1 - \frac{Y^2}{2} & -Y - sX \\ X & Y & 1 - \frac{(X^2 + Y^2)}{2} \end{pmatrix}$$
8 µas 2000-2100 
$$\begin{pmatrix} 1 - \frac{X^2}{2} & 0 & -X \\ 0 & 1 & -Y \\ X & Y & 1 - \frac{X^2}{2} \end{pmatrix}$$
0.08" 2000-2100 
$$\begin{pmatrix} X & Y & 1 - \frac{X^2}{2} \\ 0 & 0.38 & 1800-2200 \end{pmatrix}$$
0.38" 1800-2200

$$\begin{pmatrix} 1 & 0 & -X \\ 0 & 1 & -Y \\ X & Y & 1 \end{pmatrix} \quad \begin{array}{c} 0.12" \ 2000-2100 \\ 0.85" \ 1800-2200 \end{array}$$

BUT these figures assume that full-accuracy X, Y, s are used. In order to achieve significant computational savings, these quantities must themselves be approximated.

## A very approximate method

The expression:

$$GCRS \mathbf{R} CIRS \cong \begin{pmatrix} 1 & 0 & -X \\ 0 & 1 & -Y \\ X & Y & 1 \end{pmatrix}$$

where:

$$X = 2.6603 \times 10^{-7} - 32.2 \times 10^{-6} \sin \Omega$$
$$Y = -8.14 \times 10^{-14} \tau^2 + 44.6 \times 10^{-6} \cos \Omega$$

with  $\tau$  days since J2000.0 and:

$$\Omega = 2.182 - 9.242 \times 10^{-4} \tau$$
 radians

delivers 0.9 arcsecond accuracy throughout 2000-2100, which is adequate for some real-world applications.

**END** Prague, 22 August 2006 IAU 26th General Assembly JD16